

# Harnessing dislocation motion using an electric field

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Dislocation motion, an important mechanism underlying crystal plasticity, is critical for the hardening, processing and application of a wide range of structural and functional materials. For decades, the movement of dislocations has been widely observed in crystalline solids under mechanical loading. However, the goal of manipulating dislocation motion via a non-mechanical field alone remains elusive. Here we present real-time observations of dislocation motion controlled solely by using an external electric field in single-crystalline zinc sulfide—the dislocations can move back and forth depending on the direction of the electric field. We reveal the non-stoichiometric nature of dislocation cores and determine their charge characteristics. Both negatively and positively charged dislocations are directly resolved, and their glide barriers decrease under an electric field, explaining the experimental observations. This study provides direct evidence of dislocation dynamics controlled by a non-mechanical stimulus and opens up the possibility of modulating dislocation-related properties.

The modulation of mechanical and functional properties of crystalline solids based on dislocation mobility has been a central issue in materials research since the introduction of dislocation theory in the 1930s (refs. 1–3). For most crystalline solids, plastic deformation is achieved by dislocation motion. Due to their highly mobile dislocations, ductile metals can be deformed into final products through compression, tension, rolling and forging<sup>4</sup>. By contrast, ionic and covalent crystals generally suffer from poor dislocation mobility, rendering them too brittle to process using mechanical methods, and thus they are often unsuited to a broad range of manufacturing techniques<sup>5,6</sup>. The movement of dislocations also substantially affects the lifetime of semiconductor devices<sup>7</sup>, crystal growth<sup>8</sup>, solid phase transition<sup>9</sup> and the stress-induced amorphization of crystals<sup>10,11</sup>.

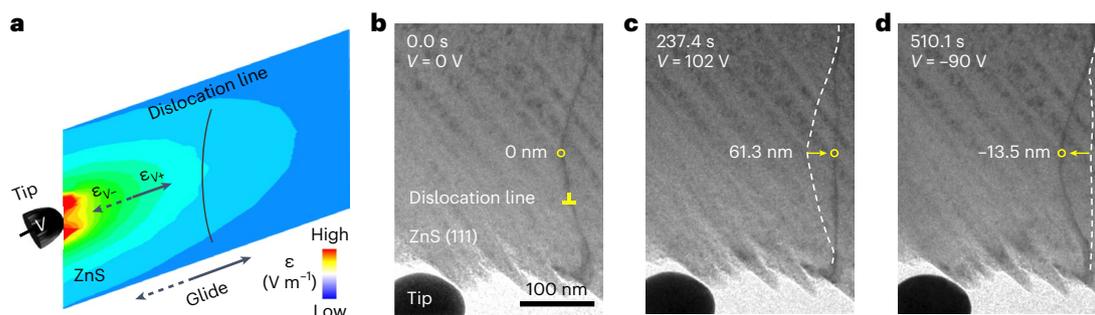
Dislocation motion is generally associated with mechanical stresses, and its related dislocation dynamics have been thoroughly studied<sup>12–15</sup>. Furthermore, extensive studies have been carried out to manipulate dislocation mobility by applying both mechanical stress

and an additional stimulus. The results of these studies show that, under mechanical loading, flow stresses can be influenced by an electric field<sup>16–19</sup> in a phenomenon known as electroplasticity<sup>16,20</sup>, or by illumination<sup>21</sup> in a phenomenon known as photoplasticity<sup>22–24</sup>. For example, the dislocation mobility of metallic, ionic and covalent crystals may be enhanced by an electric field through Joule heating, electron wind force, charged dislocations and other hypothetical effects<sup>25–27</sup>. The principal driving force of dislocation motion is, however, still mechanical stress, and this limits the processing approaches and engineering applications of many crystalline materials. Dislocation motion controlled by a non-mechanical stimulus alone is rarely expected.

Early studies on alkali halides under an electric field reported optical microscopic observation of new etching pits on alkali halides surfaces, suggesting a possible electrical response of dislocations<sup>28–30</sup>. However, to date, real-time observation of dislocation motion under an electric field has rarely been reported, and related dislocation dynamics are largely unknown. Due to recent advances, in situ transmission

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**Fig. 1 | Dislocation motion driven by an external electric field.** **a**, Schematic of the experimental set-up in TEM. A voltage  $V$  is applied to a ZnS sample through a tungsten tip.  $\epsilon$  is the applied electric field.  $\epsilon_{V+}$  indicates the electric field under a positive voltage;  $\epsilon_{V-}$  indicates the electric field under a negative voltage. **b–d**, Chronological bright-field TEM images show the positions of a dislocation as a variable voltage is applied. The initial position of the dislocation when  $V = 0$  is

in **b**. The marked point (the yellow circle) moves 61.3 nm to the right (away from the tip) when the voltage increases from 0 to 102 V (**c**). The marked point moves to 13.5 nm left to the initial position (towards the tip) when the voltage decreases to  $-90$  V (**d**). The dashed lines in **c** and **d** indicate the positions before dislocation motion. The yellow arrows show the direction of movement of the dislocation.

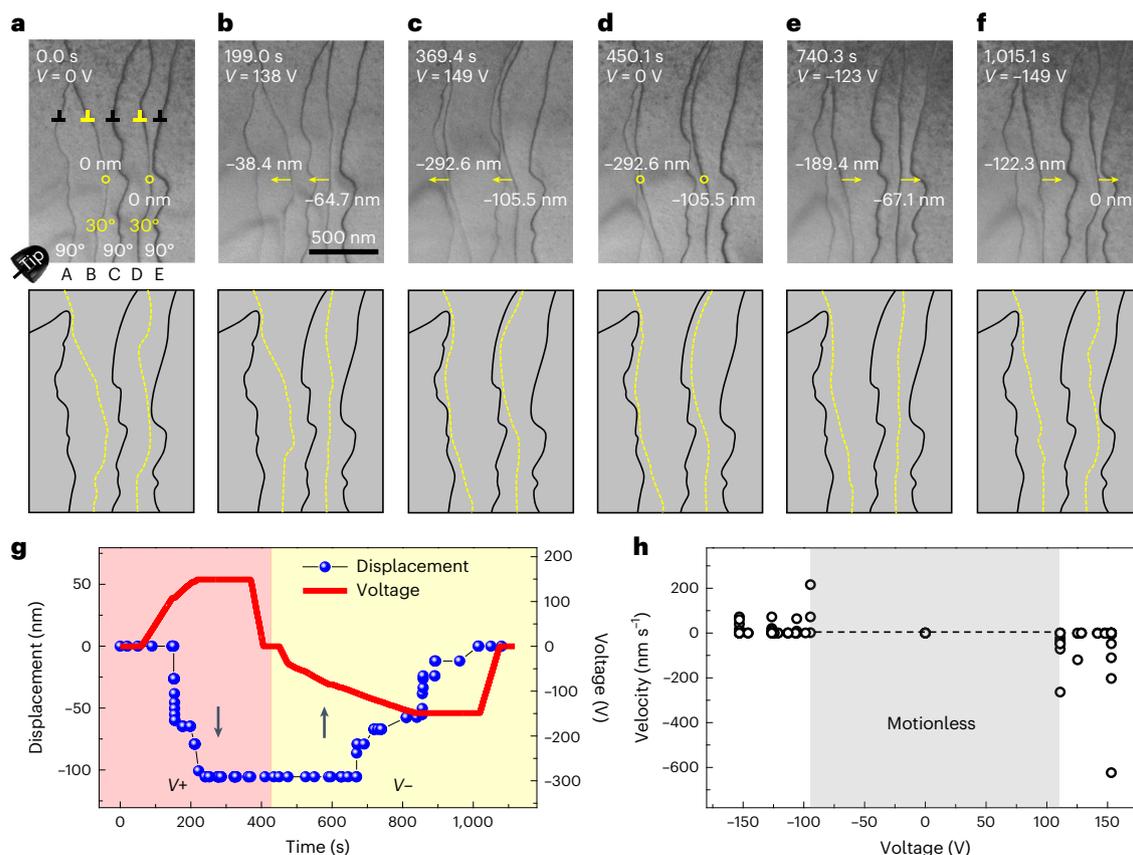
electron microscopy (TEM) has provided opportunities for visualizing crystalline defects and investigating dislocation motion in the presence of external stimuli<sup>14,31–34</sup>. For example, the movement of dislocations driven by mechanical stresses has been ubiquitously visualized in various crystals<sup>14,35</sup>. The generation and jamming of dislocation clouds by electron wind force was investigated in the phase transition material  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  (ref. 36). Also, random dislocation motion induced by electron beam irradiation was observed in graphene and GaAs (refs. 37,38). Despite these efforts, the direct probing of the dislocation motion governed by a non-mechanical stimulus has remained out of reach. In this study, the use of in situ TEM made it possible to observe that the motion of dislocations in zinc sulfide (ZnS) is driven by an external electric field. This phenomenon can be explained via the atomic-scale characterization of dislocation cores and density functional theory (DFT) calculations of the dislocation glide barriers.

Figure 1 illustrates how an individual dislocation line in a single-crystalline ZnS sample (Extended Data Fig. 1) can be subjected to an external electric field and observed in situ using TEM. As shown in Fig. 1a and Supplementary Fig. 1, a tungsten tip was used to apply a variable electric field to the ZnS sample. Initial in situ TEM testing was performed on a single  $30^\circ$  partial dislocation (Supplementary Fig. 2). As shown in Supplementary Video 1, the dislocation starts to move when the voltage reaches  $-50$  V (an electric field of  $-2.4 \times 10^7$  V m<sup>-1</sup>). The movement depends on the direction of the applied electric field: Under a positive voltage bias (Fig. 1c), the dislocation moves away from the tip; when an opposite electric field is applied, the direction of the dislocation motion is reversed, moving towards the tip (Fig. 1d). In this experiment, the dislocation moves in a reversible manner within a range of  $-82.1$  nm, reaching a maximum velocity of  $-306.4$  nm s<sup>-1</sup> (Supplementary Fig. 3).

Figure 2 shows that dislocation mobility under an electric field depends on the type of dislocations. Figure 2a displays the initial positions of two  $30^\circ$  partial dislocations (dislocations B and D, labelled at the bottom of Fig. 2a) and three  $90^\circ$  partial dislocations (dislocations A, C and E; Extended Data Fig. 2 shows the identification of these dislocations). Dislocations B and D start to move to the left when the applied voltage is above  $-100$  V (Supplementary Video 2), and they continue to move (Fig. 2b) until they are adjacent to dislocations A and C (Fig. 2c). As the voltage decreases to 0 V from the peak voltage value of 149 V, each of the five dislocations remains in the same position (Fig. 2d). When an opposite electric field is applied (Fig. 2e,f), the movements of dislocations B and D are reversed. Dislocations A, C and E remain motionless through all voltage changes. The measured displacement and applied voltage of the two marked points on dislocations B and D are plotted as functions of time (Supplementary Fig. 4 and Fig. 2g, respectively). The

maximum displacement of the marked point on dislocation B is about 292.6 nm with a velocity range of  $0$ – $623.5$  nm s<sup>-1</sup> (Supplementary Fig. 4). As shown in Fig. 2h, dislocations B and D start to move when the voltage exceeds a threshold of  $-100$  V, corresponding to an electric field of  $-5.8 \times 10^6$  V m<sup>-1</sup> applied to the dislocations (Supplementary Fig. 5 and Supplementary Table 1). The measured displacements of dislocations B and D do not exhibit a linear relationship as a function of the applied voltage due to the pinning–depinning (Extended Data Fig. 3) and kink mechanisms during motion (Extended Data Fig. 4). Due to relatively high Peierls barriers for dislocation motion in covalent crystals, their dislocations typically move by a kink mechanism<sup>39</sup>, which agrees well with our experimental observation (Extended Data Fig. 4). Furthermore, it is observed that the  $30^\circ$  dislocations in Fig. 2 move approximately against the direction of the applied electric field, while the  $30^\circ$  dislocation in Fig. 1 moves approximately along the direction of the electric field, implying opposite electrical responses. The phenomenon of electric-field-driven dislocation motion has been repeatedly observed in our experiments (Supplementary Fig. 6).

To explain the effect of an electric field on the dislocations in ZnS, the atomic structures and electronic structures of dislocation cores were characterized using atomic-scale imaging and DFT calculations. Figure 3a,b shows atomically resolved high-angle annular dark-field (HAADF) images of  $30^\circ$  S and  $30^\circ$  Zn dislocation cores with S- and Zn-terminated elements, respectively. Both cations and anions at the dislocation cores are resolved in these Z-contrast HAADF images (a brighter atomic column suggests a larger atomic number  $Z$ ; ref. 40). Figure 3c,d shows the Zn–S bond length corresponding to the circles in Fig. 3a,b, respectively. The stacking faults and dislocation cores can be located based on irregularities in the arrangements of atoms compared to the perfect lattice. The dislocation cores modify the electronic structure by introducing additional states into the crystalline band structure<sup>41,42</sup>. The density of states of the  $30^\circ$  S core has a local empty state (acceptor) close to the valence-band maximum, which tends to attract extra electrons from the Fermi sea (Supplementary Fig. 7). By contrast, the  $30^\circ$  Zn core has a local occupied state (donor) close to the conduction-band minimum, which tends to lose electrons and become positively charged. The energies of dislocations in neutral and charged states were calculated as functions of the Fermi level ( $E_F$ ) within the bandgap (Supplementary Fig. 8). Compared with the neutral states, the negatively charged  $30^\circ$  S core and positively charged  $30^\circ$  Zn core have lower calculated energies within almost the whole range of the bandgap. In other words, charged partial dislocations are energetically favourable in ZnS. Figure 3 and Extended Data Fig. 5 show the net charge distributions of  $30^\circ$  cores and  $90^\circ$  cores, respectively. The blue clouds in Fig. 3e represent the additional electrons ( $e^-$ ) localized around the



**Fig. 2 | The distinct mobility of 30° and 90° partial dislocations under an electric field.** **a–f**, Chronological bright-field TEM images and the corresponding schematics show the positions of partial dislocations during the experiment: two 30° (B and D, represented as yellow dashed lines) and three 90° (A, C and E, represented as solid black lines). The yellow arrows indicate that the marked points on dislocations B and D move to the left under a positive voltage (**b,c**) and to the right under a negative voltage (**e,f**). Dislocations A, C and E remain in their

initial positions during the entire experiment. **g**, Plots of the applied voltage and displacement of the marked point on dislocation D as functions of time. The arrows indicate the opposite directions of the dislocation motion under a positive voltage ( $V+$ , the red region) and a negative voltage ( $V-$ , the yellow region). **h**, The measured velocity of the two marked points in **a** as functions of the applied voltage. The voltage range in which the dislocations are motionless is indicated in grey.

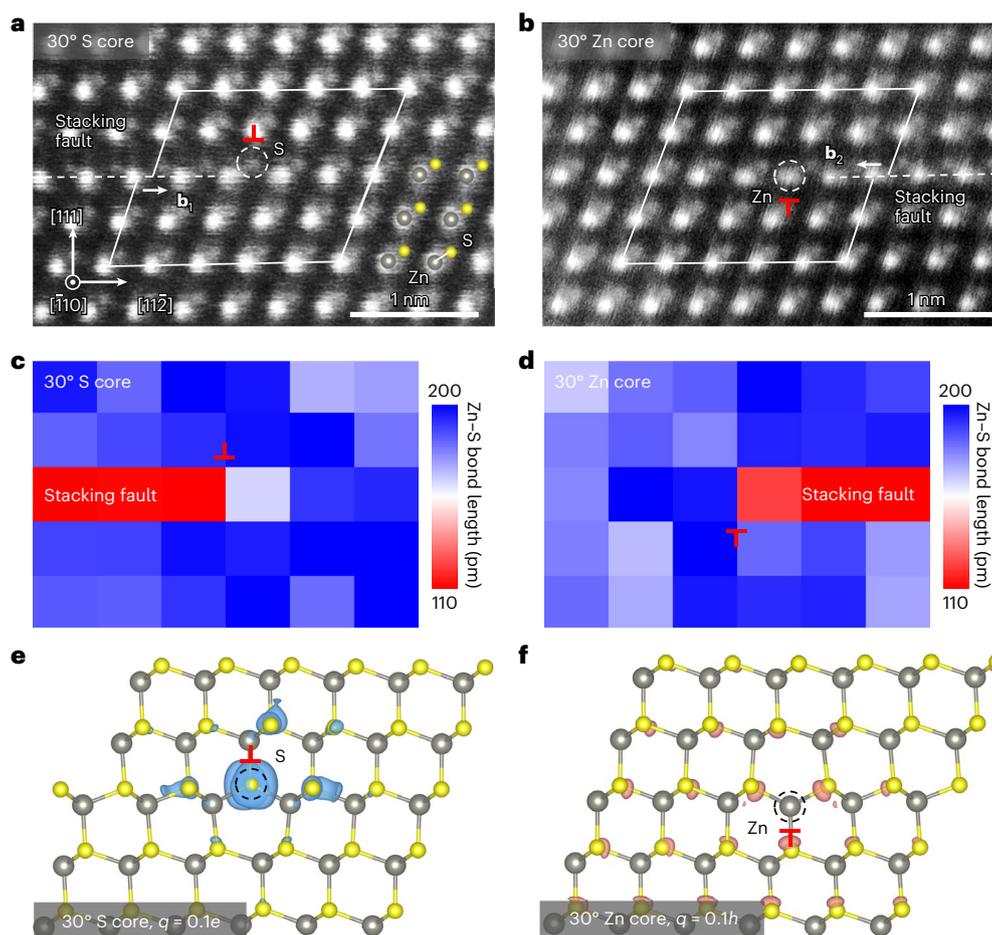
30° S core; the red clouds in Fig. 3f represent the additional holes ( $h^+$ ) around the 30° Zn core. The charged nature of the dislocations enables the manipulation of the dislocation movement using an external electric field through electrostatic interaction. Furthermore, the opposite charge states of the 30° Zn core and 30° S core (that is, the Zn core is positively charged and the 30° S core is negatively charged) may also explain the opposite movement directions of the dislocations under electric fields with the same direction, as shown in Figs. 1 and 2. The dislocation in Fig. 1 is determined to be a positively charged 30° Zn-core dislocation, because the dislocation moves along the same direction as the electric field. Dislocations B and D in Fig. 2 are determined to be negatively charged 30° S-core dislocations, because these dislocations move along the opposite direction from the electric field. We have also observed different dislocations in the same specimen moving in opposite directions under the same electric field (Supplementary Fig. 9), further verifying our charged dislocation analysis.

To further understand the mechanisms of the observed electric-field-controlled dislocation motion, the minimum energy paths (MEPs) of dislocation glide were analysed using the nudged elastic band method<sup>43,44</sup>. The MEP is the most plausible way for a dislocation to move. Figure 4a–c shows the initial, transition and final states of the glide process of a 30° S partial dislocation as viewed along the [110] and [111] directions. The thickness of our atomic models is  $\sim 0.385$  nm, which is the length of dislocation lines in our models. The glide is accompanied by the bending of a Zn–S–Zn bond in the core

region (Fig. 4b). Eventually, the dislocation moves from position 0 to position 1 (Fig. 4c). The glide processes of the 30° Zn core, 90° S core and 90° Zn core were analysed using the same method (Supplementary Fig. 10). As shown in Fig. 4d, the glide barriers ( $\Delta E$ ) of the 90° partials are higher than those of the 30° S partials, explaining that the 90° partials are sessile (Fig. 2). As discussed above, these non-stoichiometric dislocations tend to be charged; thus, the glide barrier can be altered by applying an electric field. The enthalpy of a charged system under an electric field  $\epsilon$  is modified, to first-order approximation, by the addition of a work term ( $W$ ):

$$W = \sum_i q_i \mathbf{r}_i \cdot \epsilon \quad (1)$$

where  $q_i$  and  $\mathbf{r}_i$  are the charge and Cartesian coordinates of atom  $i$ , respectively. Figure 4e shows that the barrier of the 30° S core decreases as the strength of the applied electric field increases: the barrier decreases from  $0.413$  eV nm<sup>-1</sup> to  $0.093$  eV nm<sup>-1</sup> when an electric field of  $3$  V nm<sup>-1</sup> is applied, given a net charge of  $0.5e$  where  $e$  is the electron charge. Such a small energy barrier (comparable to  $kT$  at 300 K, that is,  $-0.026$  eV, where  $k$  is the Boltzmann constant and  $T$  is the temperature) and the overall downhill trend suggest a higher probability that the 30° S partial dislocations move in this direction under the electric field. As shown in the MEPs of other dislocations (Extended Data Fig. 6 and Fig. 4f), the glide barriers of all dislocations tend to decrease under an



**Fig. 3 | Atomic structures and charge distributions of 30° partial dislocations in ZnS.** **a,b**, Atomically resolved HAADF images of 30° S (**a**) and 30° Zn (**b**) dislocation cores, viewed along the direction of the dislocation lines. The Burgers circuits in **a** and **b** show that the projected Burgers vectors  $\mathbf{b}_1$  and  $\mathbf{b}_2$  are  $a/12[11\bar{2}]$  and  $a/12[\bar{1}\bar{1}2]$ , respectively (here,  $a$  is the lattice parameter of ZnS), indicating that they are 30° partial dislocations (Extended Data Table 1). The white dashed lines indicate the locations of the stacking faults; the dashed circles indicate

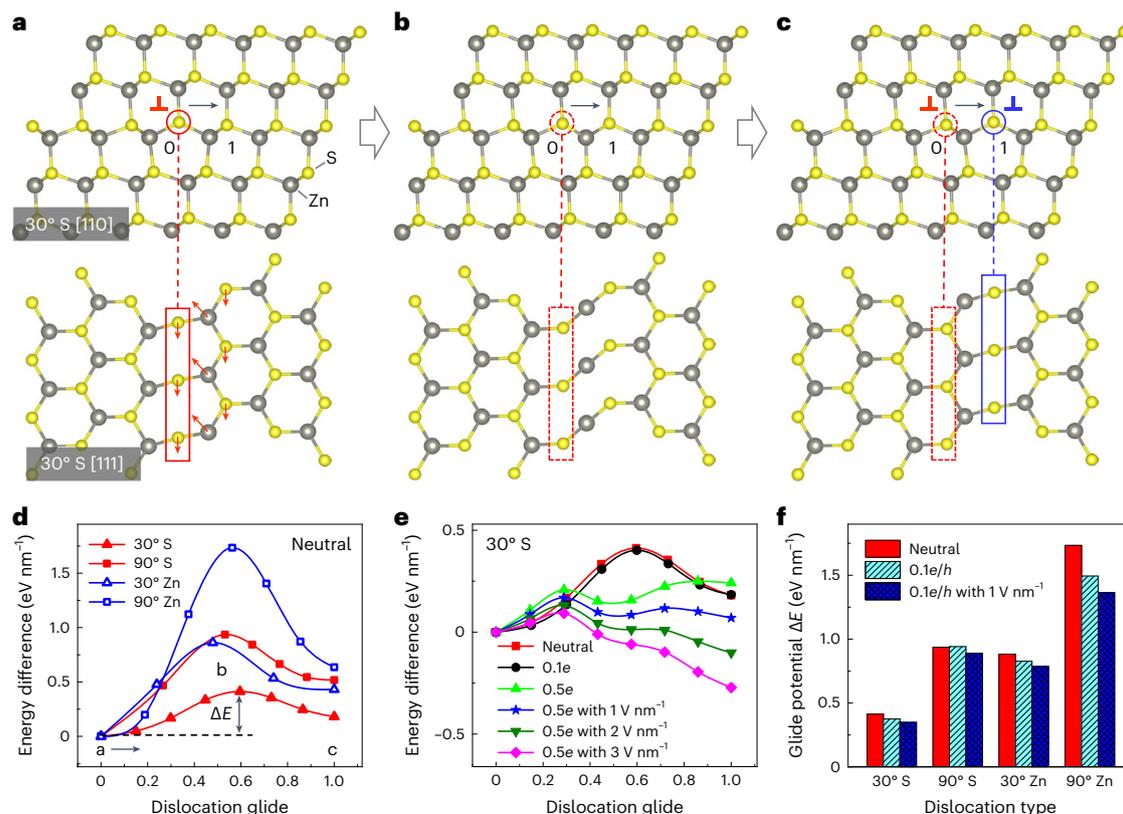
terminated elements of the dislocations. **c,d**, The Zn–S bond lengths of 30° S (**c**) and 30° Zn (**d**) dislocation cores corresponding to the circled areas in **a** and **b**, respectively. **e,f**, The net charge distributions ( $q$ ) of the 0.1 $e$ -charged 30° S core (**e**) and the 0.1 $h$ -charged 30° Zn core (**f**, where  $h$  is the charge of a hole) were obtained from the DFT calculations. The blue and red clouds represent the extra electrons and holes, respectively.

electric field, elucidating the mechanisms of electric-field-controlled dislocation motion from an energetic perspective. The DFT results show that the glide barrier of the 30° Zn-core dislocation is higher than that of the 30° S-core dislocation, which agrees well with our experiments. The estimated critical electric field required to drive the motion of the 30° Zn-core dislocation in Fig. 1 is  $-2.4 \times 10^7 \text{ V m}^{-1}$ , while that to drive the 30° S-core dislocations in Fig. 2 is  $-5.8 \times 10^6 \text{ V m}^{-1}$ . The estimated electrostatic stress on the charged dislocations is the same order of magnitude as the calculated critical resolved shear stress for the curved dislocations (Supplementary Fig. 11 and Supplementary Table 2). The electric-field-driven dislocation motion may be temperature dependent, due to the thermal fluctuation of atoms and other effects<sup>5,45</sup>. In general, the Peierls barriers of dislocations decrease with increasing temperature<sup>46</sup>, suggesting that a lower electric field is required to trigger dislocation motion at elevated temperatures.

Previous studies have reported that electrically assisted dislocation motion may result from Joule heating<sup>26</sup>, electron wind force<sup>25</sup> and charged dislocations<sup>21,47,48</sup>. Our observation of dislocations moving back and forth (Fig. 1) eliminates the Joule heating mechanism because the thermal stress arising from Joule heating is independent of the direction of the applied electric field. Our results also rule out the possibility that electron wind force plays a dominant role because

the different types of dislocations move in opposite directions under the same voltage (Figs. 1 and 2). Moreover, although irradiation by an electron beam may enhance dislocation mobility due to thermal fluctuation and other irradiation effects<sup>37,38</sup>, this motion is reported to be random, and in our study (Supplementary Fig. 12), no reversible motion was observed under electron beam irradiation (a dose of  $-30 \text{ electrons } \text{Å}^{-2} \text{ s}^{-1}$ ). Even when the electron beam is off, we still observe that the positions of the 30° dislocations are changed under an electric field (Extended Data Fig. 7 and Supplementary Video 3). Both atomic-scale characterization and DFT calculations revealed the non-stoichiometric and charged nature of dislocations in ZnS, which explains the observed dislocation motion controlled by an electric field. Charged dislocations exist in a wide range of ionic crystals and semiconductors<sup>21,49–51</sup>. Thus, our method could be expanded to other ionic and covalent crystals, especially most II–VI compounds, which exhibit relatively lower hardness and lower dislocation glide barriers than elemental and III–V semiconductors<sup>21,52</sup>.

We demonstrate that the dislocation glide barriers can be modified by altering the dislocation charge states and by applying external electric fields, enabling the plastic deformation of crystalline materials by an electric field. Our work may also offer an alternative strategy for reducing the dislocation density of semiconductors and insulators.



**Fig. 4 | Glide barriers of dislocations based on atomic structure evolution.**

**a–c**, The schematics of the initial, transition and final states of a 30° S core during the glide process, respectively. The circles and rectangles indicate the core positions viewed along the [110] and [111] axes, respectively. The dislocation core is located at position 0 in the initial state and moves to position 1 in the final state. The black arrows show the glide direction of the dislocation. The red arrows show the directions of motion of atoms around the dislocation core. **d**, MEPs of the four partial dislocations in their neutral states and **a–c**, corresponding

to Fig. 4a–c, represent the initial, transition and final states of the dislocation glide, respectively. The arrow indicates the direction of the dislocation glide. The energy of the initial state is set as the reference, indicated by the dashed line. The glide barrier  $\Delta E$  is the energy difference between the initial state and the transition state along the glide path for a unit length of the dislocation line. **e**, MEPs of a 30° S partial dislocation in various charge states and under various electric fields. **f**, The glide barriers of the four partial dislocations in neutral states (red), charged states (cyan) and charged states with an electric field (blue).

The ability to drive an individual dislocation using an electric field would allow dislocation lines to act as one-dimensional channels for tuning the properties of semiconductors and insulators. Under such circumstances, driving dislocation motion without contacting samples can be achieved (Supplementary Fig. 13). The real-time observation of dislocation motion in this study may provide a useful method for studying the dynamic behaviour of crystal defects under an electric field, opening the door to new opportunities for dislocation engineering in materials.

## Online content

Any methods, additional references, Nature Portfolio reporting summaries, source data, extended data, supplementary information, acknowledgements, peer review information; details of author contributions and competing interests; and statements of data and code availability are available at <https://doi.org/10.1038/s41563-023-01572-7>.

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## Methods

### Materials

The single-crystalline ZnS samples are commercial products from Aladdin with a purity of 99.99%. ZnS is a typical inorganic semiconductor with a sphalerite structure ( $F\bar{4}3m$ ) at room temperature. Dislocations in ZnS generally dissociate into partial dislocations due to the low stacking fault energy<sup>53</sup>. A perfect 60° dislocation with a Burgers vector  $\mathbf{b} = a/2\langle 110 \rangle$  dissociates into a 30° partial dislocation with  $\mathbf{b} = a/6\langle 112 \rangle$  and a 90° partial dislocation with  $\mathbf{b} = a/6\langle 11\bar{2} \rangle$ . A screw dislocation dissociates into two 30° partial dislocations with  $\mathbf{b} = a/6\langle 112 \rangle$ . The dissociation of 60° dislocations and screw dislocations was observed in this study (Extended Data Fig. 8). The degree of dislocation is defined as the angle between the dislocation line and the Burgers vector. Burgers vectors of perfect dislocations and partial dislocations are summarized in Extended Data Table 1. In ZnS, dislocations tend to lie on close-packed  $\{111\}$  planes along  $\langle 110 \rangle$  directions because the valley of the Peierls potential is along  $\langle 110 \rangle$  directions<sup>54</sup>.

### TEM and scanning TEM characterization

The TEM samples were prepared using the focused ion beam technique (Thermo Fisher Helios G4 UX). The ZnS was thinned using a gallium ion beam at 30 kV with a beam current from 49 nA to 7 pA. Lower accelerating voltages of 5 kV and 2 kV with a beam current from 20 to 5 pA were used for further thinning to reduce the ion beam damage. Then, a 0.5–1 kV ion beam was used for the final cleaning of specimens. Diffraction contrast TEM experiments were carried out using an FEI Tecnai F20 microscope operated at 200 kV. HAADF images were obtained using an aberration-corrected FEI Titan Cubed Themis G2 operated at 300 kV. The convergence semi-angle is 30 mrad, and the angular range of the HAADF detector is from 39 mrad to 200 mrad. Positions of Zn and S columns around dislocation cores were determined by simultaneously fitting two-dimensional Gaussian peaks<sup>55</sup>.

### In situ TEM characterization

In situ TEM experiments were carried out using an FEI Tecnai F20 microscope operated at 200 kV with a PicoFemto double-tilt TEM–STM holder from ZEPTools Technology Company. A tungsten tip acts as the top electrode to apply a bias, which was precisely controlled by a piezoelectric system. The voltage range was  $\pm 150$  V. The copper grid was grounded. The vacuum of the TEM column prevents the breakdown of air under high voltages. During the electrical tests, dislocations were imaged in diffraction contrast by using the reflection  $\mathbf{g} = \{220\}$ , as labelled in the selected area electron diffraction pattern in Supplementary Fig. 2 and Extended Data Fig. 2.  $\mathbf{g}$  is the diffraction vector of the operating reflection. Multiple beams might be selected for better brightness and contrast of dislocation lines in bright-field images. The movement processes were recorded with a OneView camera (Gatan).

### DFT simulations

We used a prism with a quadrilateral cross-section containing a single dislocation core to perform the first principles simulations. The constructed structures contain one periodic direction of  $\langle 110 \rangle$ , which is along the dislocation line, and two non-periodic directions of  $\langle 111 \rangle$  and  $\langle 112 \rangle$ . The thickness of the vacuum layer is taken to be about 14 Å to avoid elastic and electrostatic interactions between neighbouring prisms in periodic supercells. To passivate dangling bonds at the edge, pseudohydrogen atoms with a fractional charge of 1.5 and 0.5 electron charges were terminated to each Zn and S, respectively, to ensure a balanced charge. All the DFT simulations were performed using the Vienna Ab-initio Simulation Package with a plane-wave basis set<sup>56,57</sup>. The generalized gradient approximation–type Perdew–Burke–Ernzerhof functional was used for the exchange–correlation interaction<sup>58,59</sup>. The projector augmented-wave method was used for the core–valence interaction<sup>59</sup>, and the  $3s^23p^4$  and  $3d^{10}4s^2$  electrons were treated as valence states for S and Zn, respectively. The energy cut-off of 350 eV

was employed in all simulations. The energy convergence of  $10^{-5}$  eV for the electronic self-consistent field and the force criterion of  $10^{-2}$  eV Å<sup>-1</sup> were used. A  $\Gamma$ -centred ( $1 \times 2 \times 1$ ) Monkhorst–Pack K-point mesh was used in which x and z are the vacuum directions (ref. 60). In the DOS calculations, K-point mesh was enhanced to  $1 \times 51 \times 1$ . Each dislocation model contains more than 200 atoms. To avoid the influence of the artificial boundaries, we added 0.1e or 0.1h in the calculations. We studied unreconstructed dislocation cores and calculated their glide barriers, because the core reconstructions in the zinc-blende structure involve the bonding of second nearest neighbours. However, the ionic bonding in II–VI semiconductors inhibits anion–anion and cation–cation bonding and, thus, makes the core reconstructions in the ionic II–VI semiconductors less favourable compared to elemental IV–IV and III–V covalent semiconductors<sup>61–63</sup>.

### Dislocation structure energy

The energies of four dislocation structures in different charge states  $q$  were calculated using the following equation:

$$E_{\text{cal}}(\text{dislocation}, q) = E_{\text{tot}}(\text{dislocation}, q) + qE_{\text{F}}$$

where  $E_{\text{tot}}(\text{dislocation}, q)$  is the total energy of the dislocation structures in different charge states and  $E_{\text{F}}$  is the possible Fermi energy for the charged systems, ranging from the valence-band maximum to the conduction-band minimum in the perfect crystal ZnS. Particularly, the zero of the Fermi level corresponds to the valence-band maximum. In the present study, the charge states of  $q = 0.1e$  or  $0.1h$  were considered for all four types of dislocations.

### Glide barriers of dislocations

The climbing-image nudged elastic band method<sup>43,44</sup> was applied to determine energy barriers for the movement of four different types of dislocations in ZnS. The configurations before and after the dislocation movement with a unit vector were used as the initial and final configurations in the method. Energy minimization was performed for these initial and final configurations before nudged elastic band calculations. During energy minimization, the H atoms terminated at the edge were first fully relaxed while fixing the Zn and S atoms. After that, all the other atoms were relaxed while the H atoms were fixed to mimic the boundary imposed by the rest of the bulk materials. For the work term  $\sum_i q_i \mathbf{r}_i \cdot \boldsymbol{\epsilon}$ ,  $q_i$  was obtained by the Bader charge analysis<sup>64</sup>, and the summation was evaluated and added to the DFT energy for each image along the MEP. Note that only the moving atoms or the redistribution of charges contributes to the changes in the work term between images.

### Simulation of the electric fields

The distribution of an electric field in the ZnS samples was calculated by using the Ansoft Maxwell software. The tungsten tip and copper grid were assumed as perfect conductors and ZnS as an insulator with a relative dielectric constant of 8.9 (ref. 65). The tip diameter and model size were determined by TEM imaging. The tip diameter was about 80 nm in the test shown in Fig. 1 and 220 nm in the test in Fig. 2. Tip diameters influence the distribution of electric fields. The copper grid was grounded in the experiment. The distributions of electric fields under experimental bias are shown in Supplementary Figs. 1 and 5.

### Data availability

The data that support the findings of this study are available within the article and the supplementary information. Any other relevant data are also available upon reasonable request from the corresponding authors.

### Code availability

Additional data including the codes are available from the corresponding authors upon reasonable request.

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## Author contributions

Y.Z. initiated the idea, developed the research theme, supervised the project and prepared the paper outline. M.L. designed and carried out the microfabrication and experiments, analysed the data and prepared the paper draft. P.G. provided experimental support and supervision; P.X. provided guidance on the DFT calculations and discussion; and Y.S. and K.L. carried out DFT calculations under the supervision of Q.A. and P.X. All authors contributed to this work through useful discussion, revision and comments to the paper.

## Competing interests

The authors declare no competing interests.

## Additional information

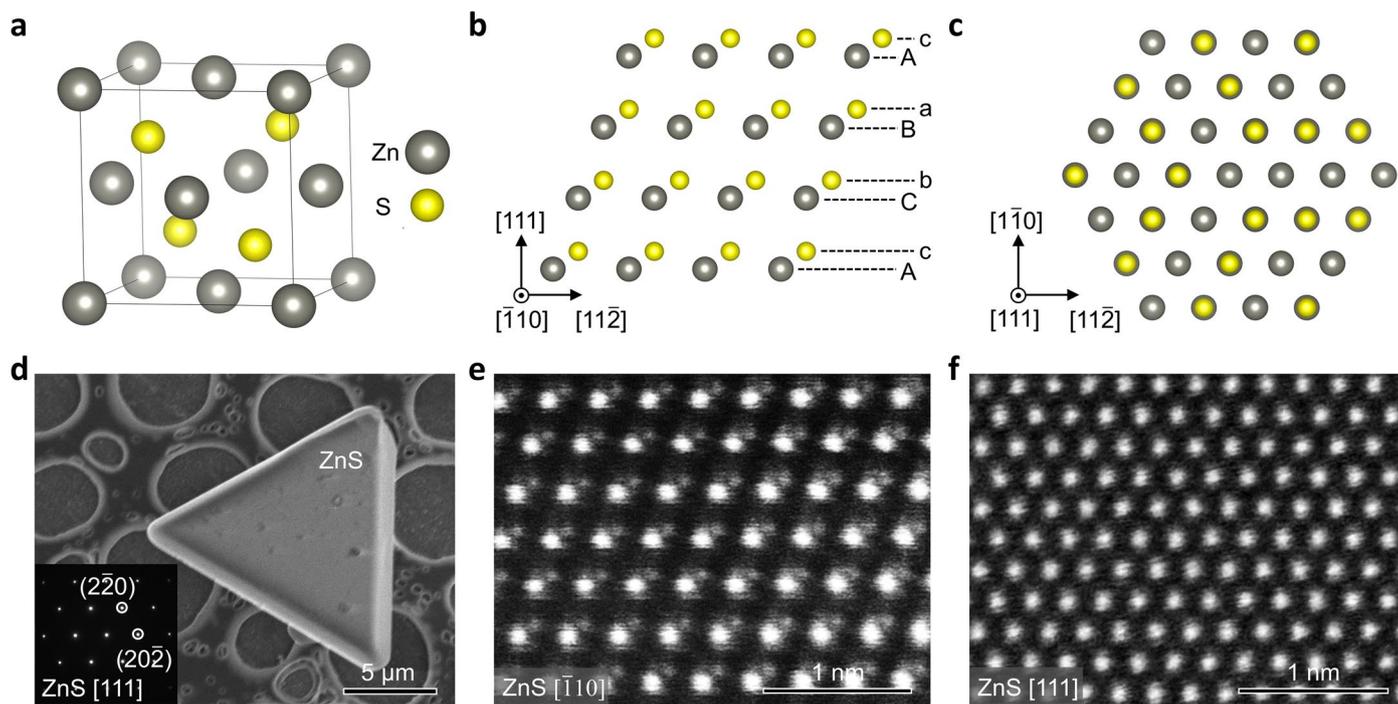
**Extended data** is available for this paper at <https://doi.org/10.1038/s41563-023-01572-7>.

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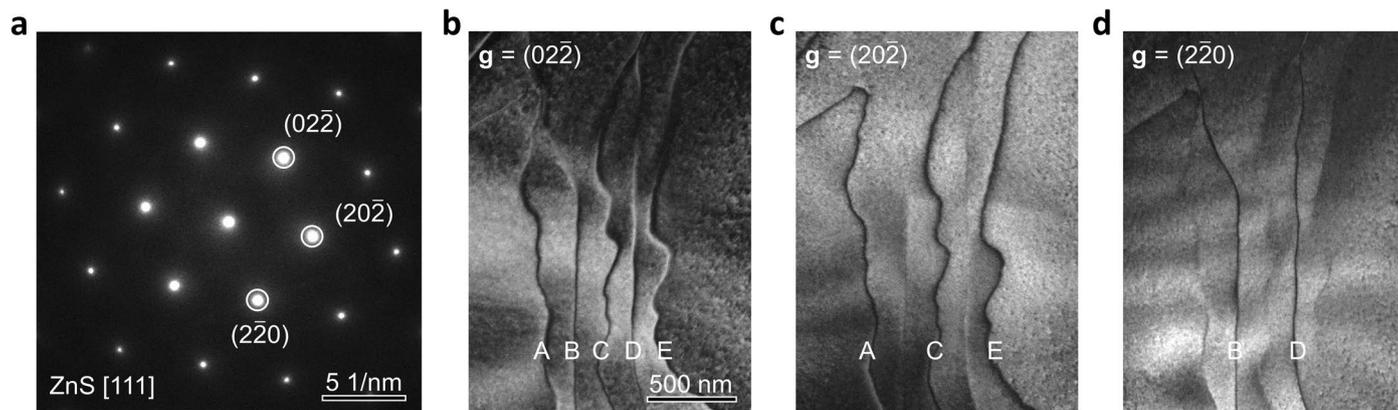
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**Extended Data Fig. 1 | Characterization of the structure of ZnS samples.**

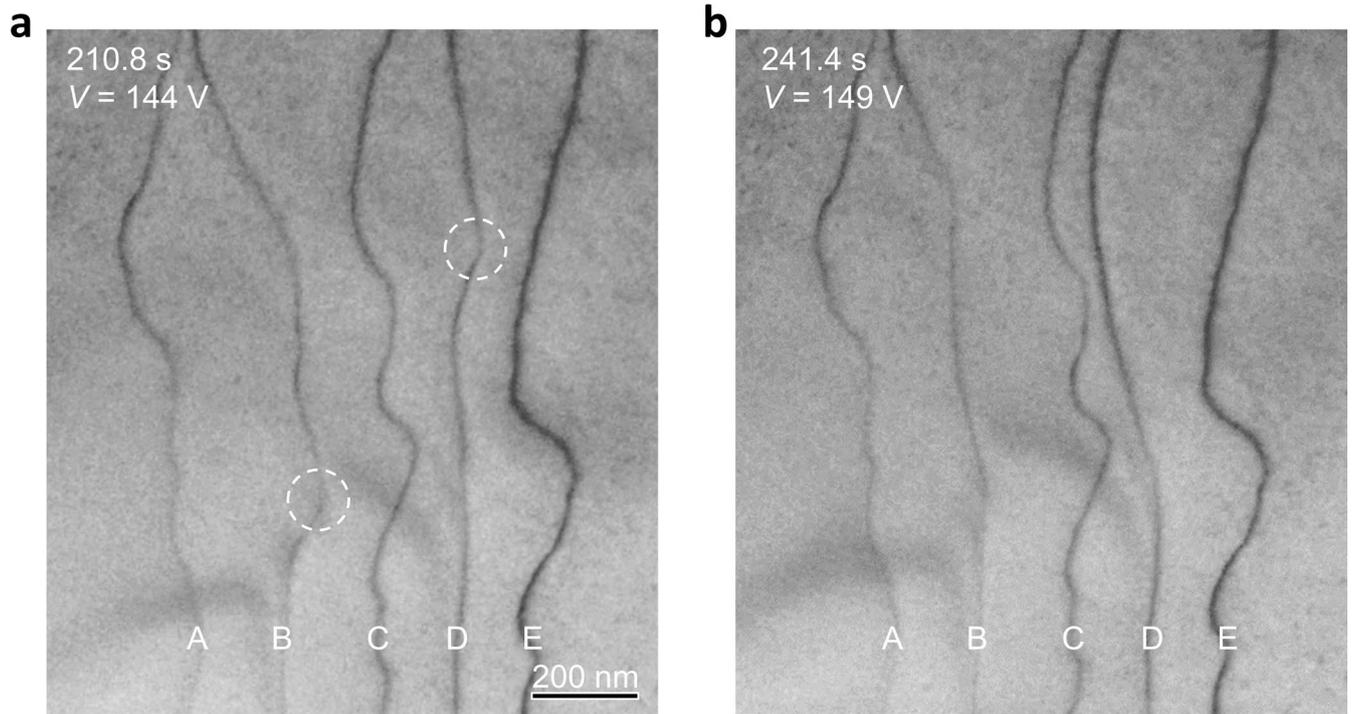
**a**, Atomic structure of sphalerite ZnS. Projections of sphalerite ZnS along the  $[\bar{1}10]$  axis (**b**) and  $[111]$  axis (**c**). **d**, Scanning electron microscopy (SEM) image of a ZnS flake

with a regular triangular shape. The edge length is about 15  $\mu\text{m}$ . The inset SAED pattern shows the single-crystalline nature of ZnS samples. Atomically resolved HAADF images of the sphalerite ZnS along the  $[\bar{1}10]$  axis (**e**) and  $[111]$  axis (**f**).

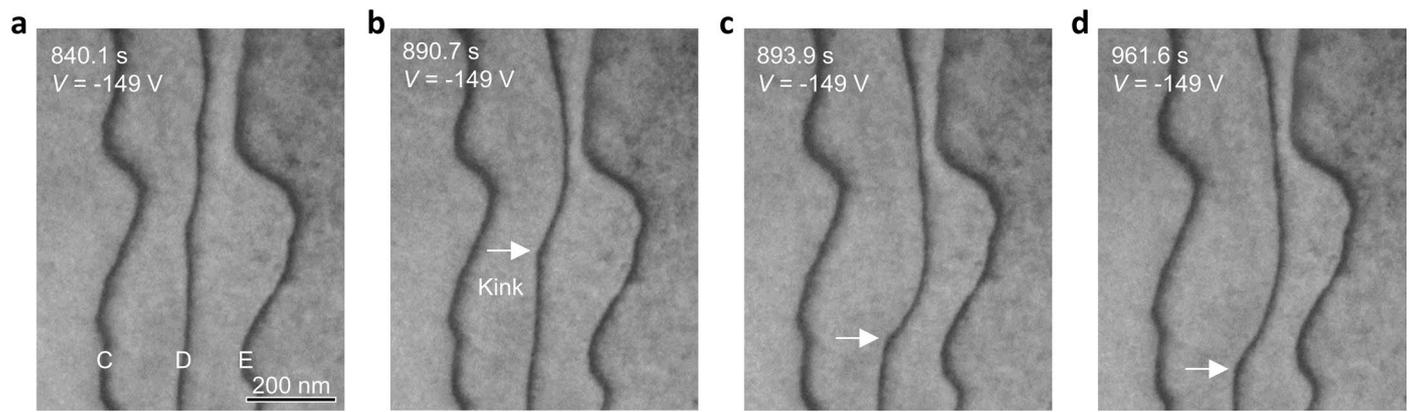


**Extended Data Fig. 2 | Characterization of Dislocations A-E in Fig. 2.** **a**, SAED pattern of the region with five dislocations in Fig. 2. Dark-field TEM images with  $\mathbf{g} = (02\bar{2})$  (**b**),  $(20\bar{2})$  (**c**),  $(2\bar{2}0)$  (**d**).  $\mathbf{g}$  is the diffraction vector of the operating reflection. Note that Dislocations B and D are invisible in **c** while Dislocations A, C, and E are invisible in **d**. Burgers vectors of dislocations are defined by the

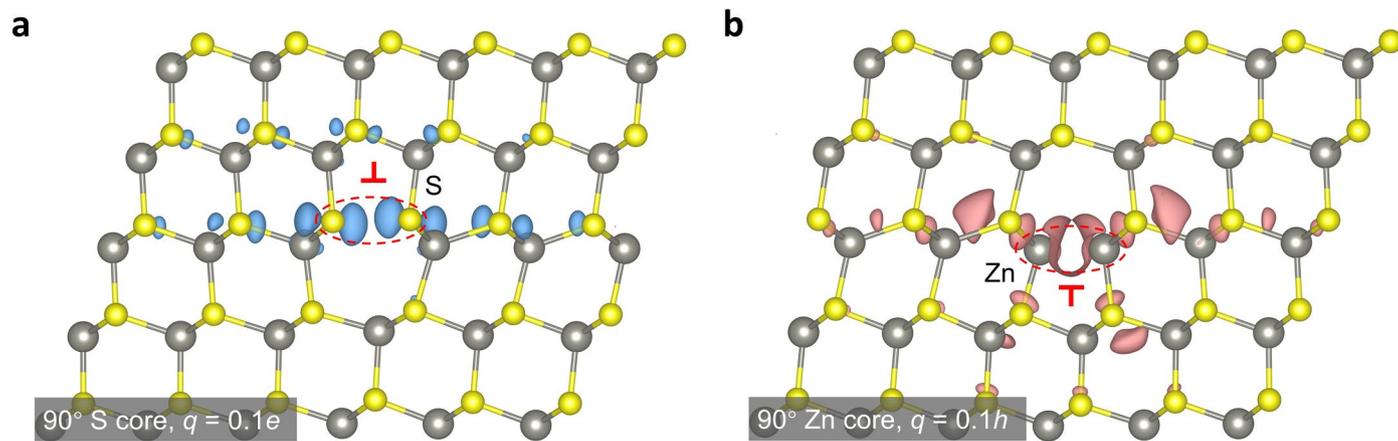
invisibility criterion  $\mathbf{g}\mathbf{b} = 0$ . Dislocations A, C and E are  $90^\circ$  partial dislocations with the Burgers vector  $a/6[11\bar{2}]$  while Dislocations B and D are  $30^\circ$  partial dislocations with the Burgers vector  $a/6[1\bar{2}1]$ . Dark points might be amorphous or dust induced by the FIB processing and absorption. The type of dislocation is determined by the angle between the dislocation line and the Burgers vector.



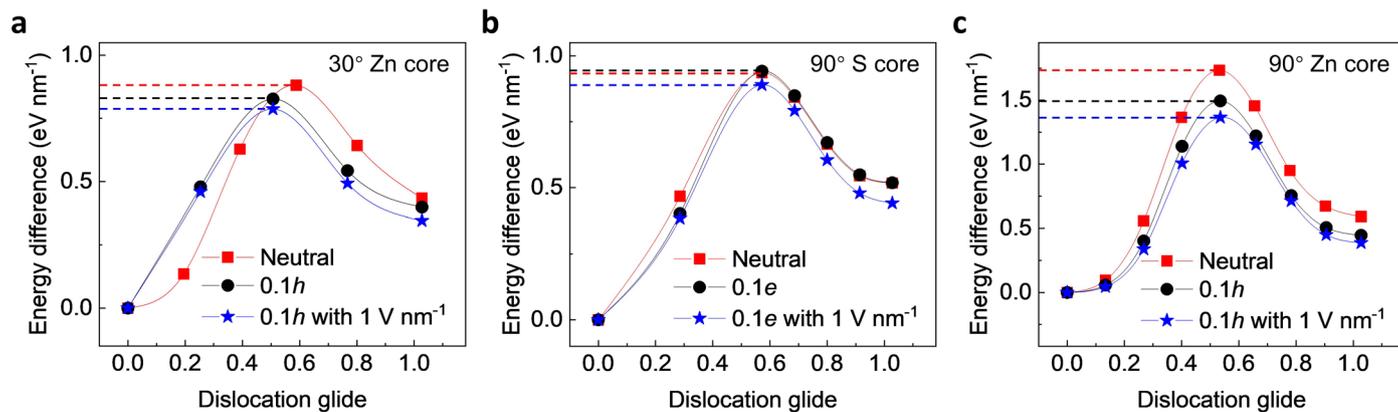
**Extended Data Fig. 3 | Pinning (a) and depinning (b) phenomena during the dislocation motion under an electric field.** White circles highlight the positions of two pinning points on Dislocations B and D.



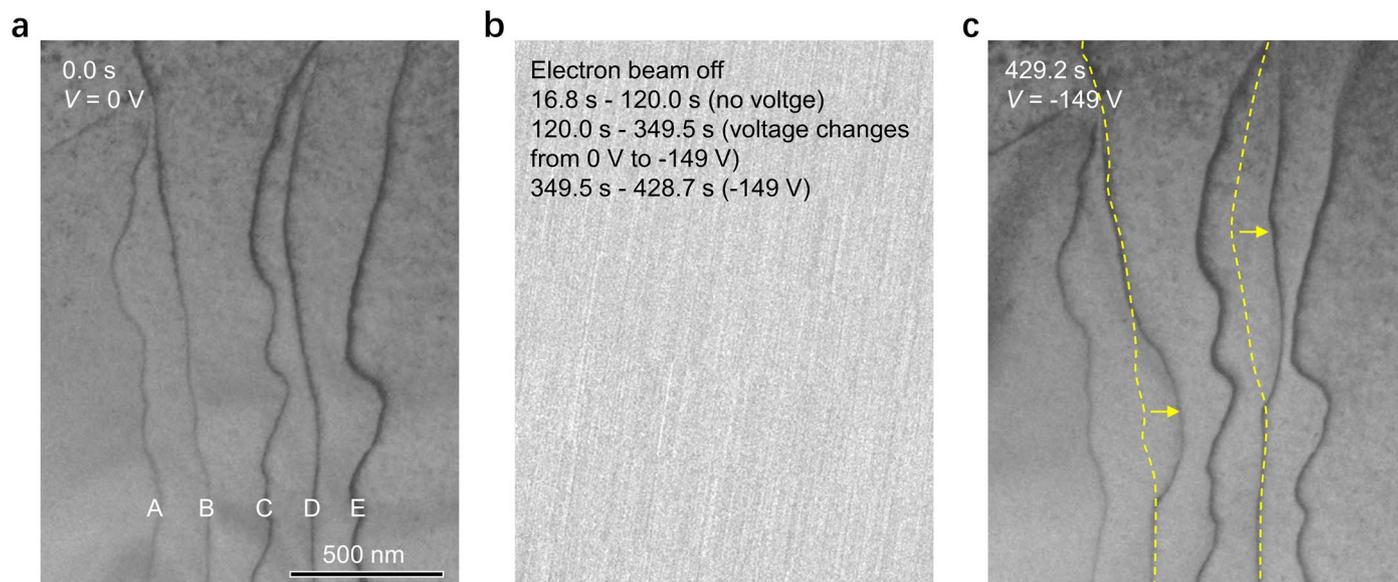
**Extended Data Fig. 4 | Kink propagation process. a-d,** Kink propagation along the dislocation line during the in situ electrical testing in Fig. 2. White arrows point to the kink positions.



**Extended Data Fig. 5 | Net charge distribution of the  $0.1e$  charged  $90^\circ$  S core (a) and the  $0.1h$  charged  $90^\circ$  Zn core (b) from DFT calculations. Blue and red clouds represent the extra electrons and holes, respectively.**

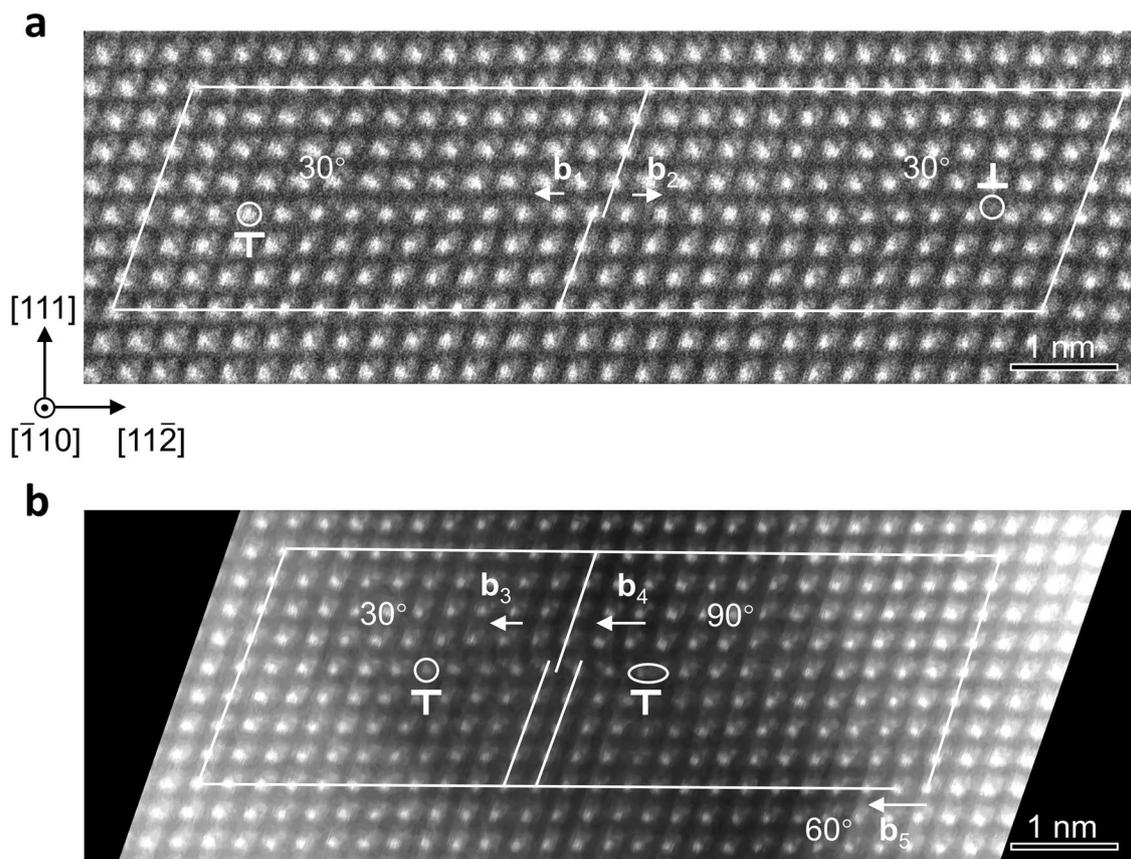


**Extended Data Fig. 6** | MEPs of charged dislocations under an applied electric field. Energy difference as a function of glide distance of the dislocations with **a**, 30° Zn core. **b**, 90° S core. **c**, 90° Zn core.



**Extended Data Fig. 7 | Dislocation motion driven by an external electric field when the electron beam is off.** **a**, The TEM image showing the initial positions of five dislocations. **b**, The electron beam is off for about 7 minutes: When the electron beam was off, the applied voltage was changed from 0 V to -149 V and

then remained at -149 V for -1.5 minutes. **c**, The TEM image shows Dislocations B and D moved away from the tip, even with the electron beam off. Dashed lines indicate the initial positions of Dislocation B and D before their motions. Arrows indicate the directions of the dislocation motions.



**Extended Data Fig. 8 | Dissociations of screw and 60° dislocations in ZnS. a,** HAADF images of a screw dislocation dissociated into two 30° partial dislocations. The closed Burgers circuit shows the overall projected Burgers vectors are zero on the  $(\bar{1}10)$  plane, indicating these two partial dislocations are dissociated from a screw dislocation.  $\mathbf{b}_1$  and  $\mathbf{b}_2$  indicate the projected Burgers vectors of left and right partial dislocations are  $a/12[\bar{1}\bar{1}2]$  and  $a/12[1\bar{1}\bar{2}]$ , respectively. White circles indicate terminated elements of dislocations cores.

This is a stacking fault between two partial dislocations. Scale bar, 1 nm. **b,** HAADF images of a 60° dislocation dissociated into one 30° dislocation and one 90° partial dislocation.  $\mathbf{b}_3$  and  $\mathbf{b}_4$  indicate the projected Burgers vectors of left and right partial dislocations are  $a/12[\bar{1}\bar{1}2]$  and  $a/6[\bar{1}\bar{1}2]$ , respectively. The Burgers circuit shows the overall projected Burgers vector  $\mathbf{b}_5$  is  $a/4[\bar{1}\bar{1}2]$  on the  $(\bar{1}10)$  plane, indicating these two partial dislocations are dissociated from a 60° dislocation. There is a stacking fault between the two partial dislocations. Scale bar, 1 nm.

Extended Data Table 1 | Dislocation types and corresponding Burgers vectors in ZnS

|                      | Dislocation type    | Burgers vector <b>b</b>  | Projection of <b>b</b> on {110} |
|----------------------|---------------------|--------------------------|---------------------------------|
| Perfect dislocations | 60°                 | $a/2\langle 110 \rangle$ | $a/4\langle 112 \rangle$        |
|                      | Screw               | $a/2\langle 110 \rangle$ | $a/4\langle 112 \rangle$        |
| Partial dislocations | 30° (S or Zn cores) | $a/6\langle 112 \rangle$ | $a/12\langle 112 \rangle$       |
|                      | 90° (S or Zn cores) | $a/6\langle 112 \rangle$ | $a/6\langle 112 \rangle$        |

Perfect dislocations in ZnS include 60° and screw dislocations with the Burgers vector  $a/2\langle 110 \rangle$ ; Partial dislocations in ZnS include 30° and 90° dislocations with the Burgers vector  $a/6\langle 112 \rangle$ , where  $a$  is the lattice parameter.